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# CHARACTERISTIC OF HYDROGEN PRODUCTION FROM COAL TAR WITH HIGH TEMPERATURE AND HIGH PRESSURE WATER

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## ABSTRACT

A steam gasification method of "HyPr-RING" is a new hydrogen production process from organic matters such as coal, biomass and waste with high temperature and high pressure water and calcium-based CO<sub>2</sub> sorbent. In this study, the gasification characteristic of tar was investigated using a small batch reactor heated in a fluidized sand bath. As a result, CH<sub>4</sub> and H<sub>2</sub> were mainly produced from tar as well as coal. The amounts were decreased but the ratio of CH<sub>4</sub> to H<sub>2</sub> in product gas was increased with decreasing temperature. The predominant production was in the initial stage including heating period. The behavior for the tar is similar to that for coal, suggesting that the CH<sub>4</sub> and H<sub>2</sub> production from coal in the initial stage should be caused by tar in coal and especially, H<sub>2</sub> production in the second stage should be by char in coal. These results indicate that tar discharged above the bed is reduced as much as possible, when the coal gasification as the HyPr-RING is carried out in a fluidized bed reactor, and that CH<sub>4</sub> production from tar remained in the bed is reduced and H<sub>2</sub> production by catalytic reaction or polymerization of tar is promoted in the bed.

## KEYWORDS

Hydrogen production, Coal tar, CO<sub>2</sub> sorbents, Gasification, High pressure steam

## INTRODUCTION

The utilization of hydrogen energy is one of most available method to reduce the environmental impact and the hydrogen production of coal is one of the clean coal technologies. The HyPr-RING (Hydrogen Production by Reaction Integrated Novel Gasification) is a new gasification method to produce hydrogen from hydrocarbon resources such as fossil fuel, biomass and waste with the high temperature and high pressure steam and simultaneously to reduce CO<sub>2</sub> by calcium-based sorbent<sup>1)</sup>.

Figure 1 shows the concept of HyPr-RING method. Almost all of organic materials such as coal can be reacted with steam and sorbent to produce mainly H<sub>2</sub> and CaCO<sub>3</sub>. CaCO<sub>3</sub> can be regenerated to CaO by calcinations and CO<sub>2</sub> in high concentration can be collected. It starts being developed with a continuous bench-scale unit with a fluidized bed reactor.

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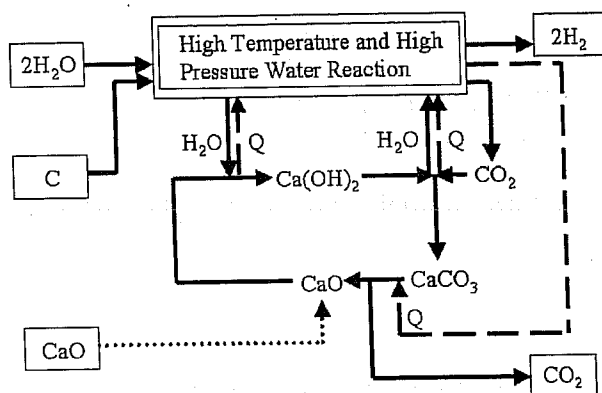


Fig.1 Concept of HyPr-RING method.

Objective of this study is to clear the behavior of tar produce in the initial stage of coal gasification, which would be devolatilized with pyrolysis reactions during heating period of coal particles even in the fluidized bed. The tar would produce  $\text{CH}_4$  as a by-product together with  $\text{H}_2$  as a target product. In this study we are focusing on the  $\text{CH}_4$  production from the tar in the initial stage reaction.

## EXPERIMENTAL

In the present study, tar of Taiheiyo-coal (Japanese subbituminous coal) was used as a tar sample and it was gasified with steam under the condition of temperatures of 873 to 973 K and pressure of 19.8 MPa (subcritical condition) using a tubing-bomb micro-reactor (TB reactor).

### Tar sample

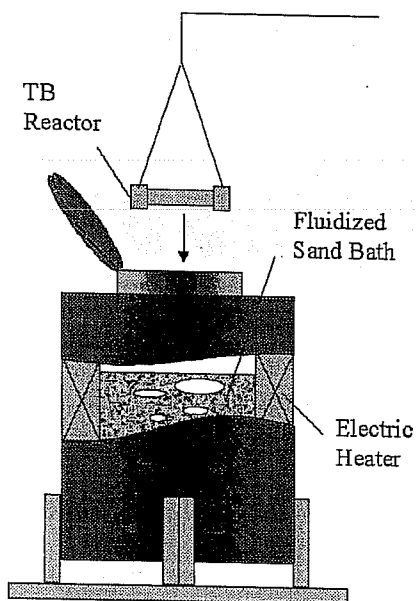
Tar was made by thermal cracking of Taiheiyo-coal at 873 K for 2 hour in  $\text{N}_2$  flow. The chemical property is shown in Table 1. As a  $\text{CO}_2$  sorbent, reagent grade  $\text{Ca}(\text{OH})_2$  of Nacalai tesque, Kyoto, Japan was used.

Table 1 Chemical property of Taiheiyo-coal tar.

Proximate analysis (dry) [wt%]				Ultimate analysis (daf) [wt%]			
VM	FC	Ash	Moist.	C	H	N	O, S (dif.)
98.10	1.46	0.46	0.00	75.50	9.74	0.59	14.17

### Experimental Conditions and Apparatus

Experimental conditions and apparatus are shown in Fig. 2. A TB reactor was a seamless tube of 100 mm long, O.D. 12.7 mm, an internal volume of  $7.2 \text{ cm}^3$ , which was made of stainless steel (SUS-316). The reactor was sealed at both ends with SUS-316 caps. It was externally heated to the desired temperatures with a fluidized sand-bath heater, whose inner diameter was 400 mm, bed height was 450 mm, and bed material was silica sand.



### Tube Reactor

- Seamless Tube Made of SUS-316
- Length = 100 mm
- Outer Diameter = 13 mm
- Inner Diameter = 9 mm
- Sealed at Both Ends with SUS-316 Caps.
- Inside Volume = 7.2 cm<sup>3</sup>

### Fluidized bed sand bath

- Inner Diameter = 400 mm
- Bed Heater = 450 mm
- Bed Material: Silica Sand

Fig. 2 Experimental conditions and apparatus

### Experimental Procedure

A mixture of tar, distilled water and Ca(OH)<sub>2</sub> was put into the TB reactor with nitrogen. The TB reactor was soaked in the fluidized sand bath, rapidly heated and hold at 873 to 973 K. The mixing ratio of the tar, sorbent and water is shown in Table 2.

Table 2 Mixing ratio of the tar, sorbent and water.

	Pressure	Tar	Ca(OH) <sub>2</sub>	Water	H <sub>2</sub> O/C	Ca/C
873 K	19.8 MPa	0.062 g	0.407 g	0.407 cm <sup>3</sup>	5.9	1.4
923 K		0.057 g	0.376 g	0.376 cm <sup>3</sup>		
973 K		0.060 g	0.350 g	0.350 cm <sup>3</sup>		

As confirmed in our previous research<sup>2)</sup>, the TB reactor with a less heat capacity can be more rapidly heated up to a desired temperature than a conventional autoclave. The average heating rate was about 330 K/min and it took about 2 minutes under the present heating conditions. The measurement temperature and pressure in the reactor corresponded to calculation results estimated by the sand bath temperature and the amount of water in the reactor.

After gasification, the reactor was quickly pulled up from the sand bath, and it was rapidly cooled down to room temperature with water to quench the reaction. Produced gases were collected by the water substitution method<sup>2)</sup> and the volume of the gas was measured with a graduated cylinder. The compositions of collected gas, H<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub>, CH<sub>4</sub>, CO, CO<sub>2</sub>, C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> were analyzed by TCD-micro gas chromatographs (Aera, model M200; (1) with MS-5A and PPQ columns and Ar carrier gas, (2) with a PPU column and He carrier gas).

## RESULTS AND DISCUSSION

### Changes of Gas yields from Tar with Reaction Time

First of all, coal conversions to gases are shown in Fig. 3. It was about 40% at 2 min and 60% at 30 min. Yields of gas produced from the coal and the steam are shown in Fig. 4 together with product gas yields from char and tar as reactants. From these figures, it can be seen that in the condition of the HyPr-RING methods by using the TB reactor, which enabled rapid heating, the composition of product gas from coal is strongly dependent on the initial stage of gasification or pyrolysis reaction until 5 minutes.

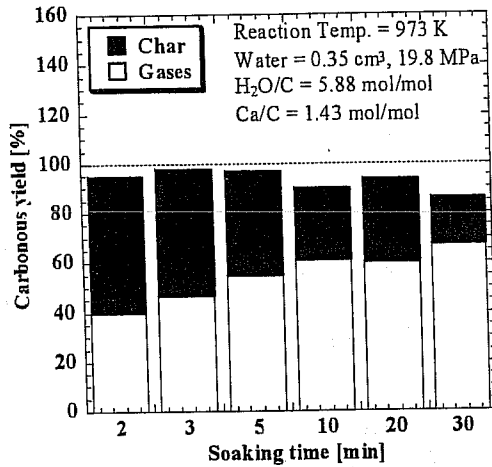


Fig. 3 Coal conversions to gas at 973K.

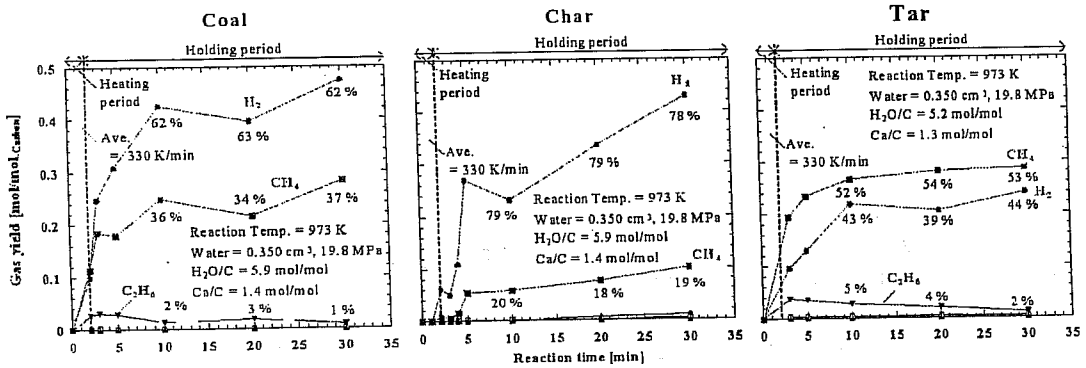


Fig. 4 Changes of yield of CH<sub>4</sub> and H<sub>2</sub> produced from coal, char and tar with reaction time at 973 K

Carbon source of hydrogen production with the reaction of coal and stem is divided roughly into char and tar. The char is mainly converted into H<sub>2</sub> and the tar into CH<sub>4</sub> and H<sub>2</sub>. Objective of the HyPr-RING is to produce H<sub>2</sub>, which means that CH<sub>4</sub> is a by-product. Because CH<sub>4</sub> production took place in the initial stage when tar was used as a reactant, CH<sub>4</sub> production in the initial stage when coal was used should be due to the tar in coal.

The dependence of CH<sub>4</sub> production on the gasification temperature is shown in Fig. 5. The amount of CH<sub>4</sub> was decreased with decreasing temperature but the ratio of the yields of CH<sub>4</sub> to H<sub>2</sub> was increased, as 53/44 at 973 K and 60/22 at 873K.

Additionally, at 873 and 973 K, C<sub>2</sub>H<sub>6</sub> was also produced and CO<sub>2</sub> was little. In the heating period and the initial stage within 5 minutes, the yields of H<sub>2</sub>, CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> produced from the tar were rapidly increased. The rapid production should be caused by the thermal cracking and gasification of tar. After 5 minutes, the yields of H<sub>2</sub>, CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> were not significantly increased with reaction time. If the remained tar was partially polymerized to the reactive char, it would produce much more H<sub>2</sub> with the reaction of the char and steam. Furthermore, a little of increase of CH<sub>4</sub> might be due to production of the reactive char and

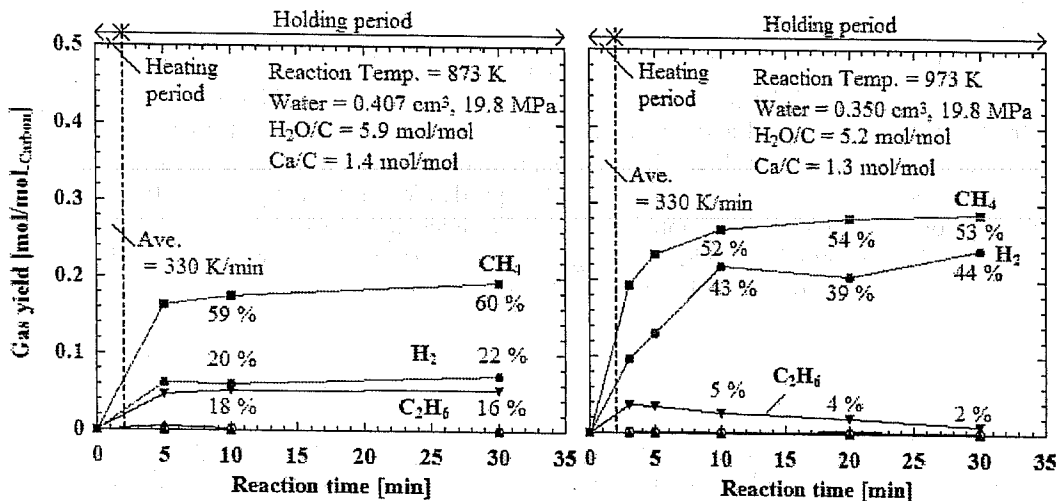


Fig. 5 Comparison of gas yields of CH<sub>4</sub> and H<sub>2</sub> produced from tar at 873 and 973 K.

the following reaction<sup>3)</sup>:



Consequently, even if tar changes into char, it seems not so reactive or not so much amount in the present experimental conditions. On the other hand, C<sub>2</sub>H<sub>6</sub> was slowly decreased after 3 min at 973 K. It suggests that a part of hydrocarbon might participate in the H<sub>2</sub> and CH<sub>4</sub> production after 5 minutes.

### Changes of H<sub>2</sub> and CH<sub>4</sub> Produced from with Reaction Temperature

As previously described on the dependence of temperature on yields of the produced gases, the ratio of the yields of CH<sub>4</sub> and H<sub>2</sub> was increased. The yields from tar at 30 min are plotted as a function of reaction temperature in Fig. 6.

Both yields of H<sub>2</sub> and CH<sub>4</sub> were linearly increased with reaction temperature. In addition, the production rate of H<sub>2</sub> is higher than that of CH<sub>4</sub>. This might suggest a possibility that increase of H<sub>2</sub> production in the second stage is due to the char produced from tar and steam as following reaction:

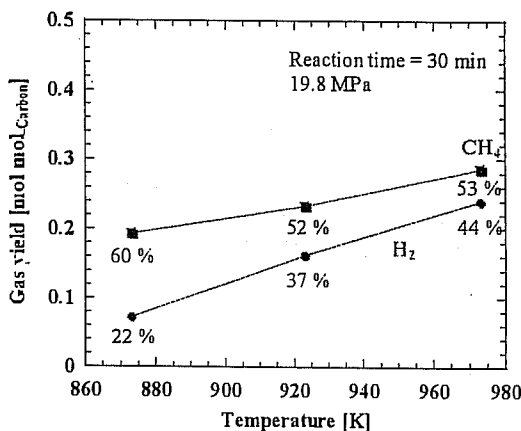
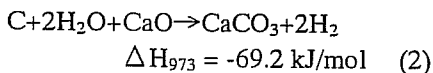


Fig. 6 Changes of gas yields of H<sub>2</sub> and CH<sub>4</sub> from tar for 30 min with reaction temperature.

## Application to Fluidized Bed Reactor

As previously described, the HyPr-RING project will be developed with a continuous bench-scale fluidized bed reactor. Coal particles fed into the fluidized bed reactor produce tar during the heating period and the initial stage of gasification with steam, which is discharged into the freeboard above the bed and causes tar trouble or carbon loss. The tar production should be reduced as much as possible. In addition, if  $\text{CH}_4$  produced from tar is needless, tar in the bed should be reduced and selective  $\text{H}_2$  production by catalytic reaction or polymerization of tar should be promoted in the bed. Since tar is easily produced at low temperature, heating by passing rapidly through the low temperature period and coking reaction by deposition of tar on the bed material at high temperature should be available.

## CONCLUSIONS

To understand of the reaction mechanism and the role of tar to produce rich hydrogen by the HyPr-RING method, we studied on tar gasification by using micro reactor under the high pressure and temperature steam and obtained the following conclusions;

- (1)  $\text{H}_2$  and  $\text{CH}_4$  are mainly produced from tar, and increased with reaction time. The yield of  $\text{H}_2$  is lower than that of  $\text{CH}_4$ .
- (2) The yields of  $\text{H}_2$  and  $\text{CH}_4$  are increased with reaction temperature, which are rapidly produced in the initial stage. The increasing rate in the second stage after 5 minutes is increased with reaction temperature.
- (3) Behavior of  $\text{CH}_4$  production in the initial stage of coal gasification is similar to that of tar gasification.

## ACKNOWLEDGEMENTS

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