

# Optimum conditions of selective non-catalytic reduction by activated ammonia generated by DBD pulsed plasma

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**Abstract**—Selective non-catalytic reduction of NO<sub>x</sub> by activated ammonia injection has been developed to broaden and lower the narrow temperature window for de-NO<sub>x</sub>. A temperature window enlargement of 150 °C was achieved at the lower boundary of the window using activated ammonia injection. Hydrogen played a key role in the expansion of the temperature window in activated ammonia injection. The purpose of the present study was to investigate an optimum condition to improve the efficiency of De-NO<sub>x</sub>. The optimum conditions of de-NO<sub>x</sub> reactions was investigated by using an NH<sub>3</sub>/H<sub>2</sub> gas mixture in the temperature range of 500°C—750 °C. The optimum conditions of de-NO<sub>x</sub> reaction changed by the reaction temperature. The biggest NO<sub>x</sub> removal efficiency didn't change with the reaction temperature in an optimum, and it was 80% in NH<sub>3</sub>/NO = 1.0.

**Keywords**—DeNO<sub>x</sub>, SNCR, Hydrogen

## I. INTRODUCTION

Recently, the establishment severe NO<sub>x</sub> concentration control of discharge starts to be put into effect for an area agreement, and which is de-NO<sub>x</sub> equipment is being needed combustion facility of the small-to-medium-sized scale of the waste incinerator. Selective non-catalytic reduction (SNCR) is wished for in a face of the installation area and the equipment cost at a burning furnace of the small-to-medium-sized scale. But there is a reaction temperature range in SNCR in a high-temperature range of 850-1175 °C (as Temperature window) <sup>(1)</sup>, reaction time by a high-temperature range can't be secured sufficiently by a burning hearth and an incinerator of the small-to-medium-sized scale, and there is a problem that NO<sub>x</sub> removal efficiency falls. It's desirable to install SNCR equipment in a hearth exit by an incinerator, but the hearth exit temperature is the 750 °C degree, and it isn't possible to apply SNCR. The plan into which Temperature window is expanded on the cold side is necessary for a solution of these problem. Temperature window magnifies 150 °C on the cold side with to inject the NH<sub>3</sub> excited by atmospheric pressure plasma (dielectric barrier discharge: DBD) in an exhaust gas<sup>(2)-(3)</sup>. There is a possibility that a burning hearth of the small-to-medium-sized scale and SNCR for incinerators can be established by using the ammonia reformed in DBD (as Reforming ammonia SNCR).

From the former study, we inferred that H<sub>2</sub> was the reforming ammonia chemical kind which makes promote de-NO<sub>x</sub>. The purpose of this research was to make the de-NO<sub>x</sub> effect of H<sub>2</sub> clear and confirm the optimum of de-NO<sub>x</sub> by H<sub>2</sub> addition. It was investigated about a change in the NO<sub>x</sub> removal efficiency when adding H<sub>2</sub>.

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## II. METHODOLOGY

Fig. 1 shows experimental setup for SNCR with hydrogen addition. Equipment consists of model gas supply system, de-NO<sub>x</sub> gas supply system, preheating department, gas mixture office, reaction department, gold furnace and NO<sub>x</sub>, N<sub>2</sub>O, analysis installation. Gold furnace can do temperature control of a preheating department and a reaction independently respectively.

The gas to which the oxygen density (8.2%), the NO density (500ppm), the NH<sub>3</sub> density (400 – 500 ppm) and the general flow rate (3.0 L/min fixing) were adjusted by a mass flow controller with a gas blender was supplied from the preheating part side. H<sub>2</sub> was injected in the gas mixture part, and after mixing with model gas, a Thermal reaction has been caused in the reaction part. The temperature of the reaction part was heated from 600 °C to 750 °C and the temperature was made regular. The pressure in the system was controlled in the atmospheric pressure neighborhood (103.1 ± 0.1 kPa) by the style pressure equipment.

After removing slip ammonia by an adhesion pill during dense fog so as not to affect an analyzer, the gas treated with hydrogen addition introduced into a NO<sub>x</sub> meter and N<sub>2</sub>O meter by a gas sampler with a pump and analyzed continuously. NO<sub>x</sub> removal efficiency was asked by gauging the density of NO in the reaction part temperature 500 °C ([NO]<sub>in</sub>) and the density of NO of whole exit gas in each experimental conditions ([NO]<sub>out</sub>) with NO<sub>x</sub> total (Eq. 1).

$$\text{NO removal} = ([\text{NO}]_{\text{in}} - [\text{NO}]_{\text{out}}) / [\text{NO}]_{\text{in}} \times 100 \quad \text{Eq. 1}$$

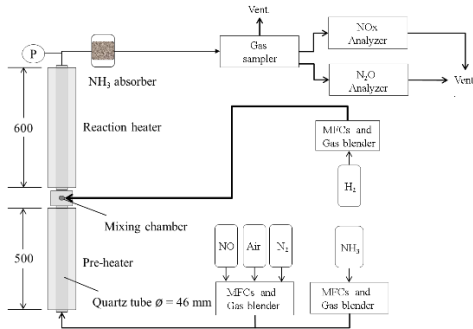


Fig. 1 Schematic diagrams of hydrogen addition De-NOx experimental apparatus

### III. RESULTS

Fig. 2 shows Characteristics of NO<sub>x</sub> removal by hydrogen addition SNCR when NH<sub>3</sub>/NO molar ratio ( $M_{R1}$ ) = 1.0. NO<sub>x</sub> removal efficiency rose by addition of hydrogen. While it was NO<sub>x</sub> removal efficiency 50% at H<sub>2</sub>/NH<sub>3</sub> molar ratio ( $M_{R2}$ ) = 0, in which temperature range did NO<sub>x</sub> removal efficiency also even rise in 80% by addition of hydrogen. NO<sub>x</sub> removal efficiency was rose by increasing H<sub>2</sub> addition amount, and after becoming biggest, it was fixed. When being equivalent in the price of the  $M_{R1}$ , the one with the high reaction temperature becomes small in the necessary hydrogen quantity. I can think you can get high NO<sub>x</sub> removal efficiency by adding H<sub>2</sub> beyond the most suitable H<sub>2</sub> amount when the amount of the NH<sub>3</sub> is more fixed than this thing.

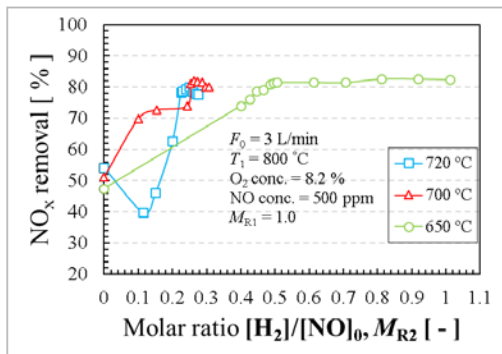


Fig. 2 Characteristics of NO<sub>x</sub> removal by hydrogen addition SNCR

Fig. 3 shows the tendency of the optimum hydrogen amount in hydrogen addition de-NOx. It becomes so little that the price of  $M_{R1}$  is big in the same temperature range. The optimum conditions respectively by the value of  $M_{R1}$  and the temperature range. Therefore, it's important to will can find the optimal condition in the respective temperature range and  $M_{R1}$  for practical use.

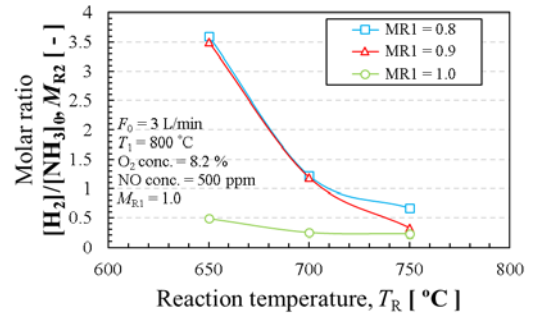


Fig. 3 The tendency of the optimum hydrogen amount in hydrogen addition de-NOx.

Fig. 4 shows comparison of the biggest NO<sub>x</sub> removal efficiency in the optimum condition. Addition of activated ammonia by plasma or H<sub>2</sub> made the reaction temperature range expand to the cold side. Addition of the optimum hydrogen added the de-NO<sub>x</sub> efficiency of more than 80 % of NO<sub>x</sub> removal efficiency in reaction temperature range more than 650 °C.

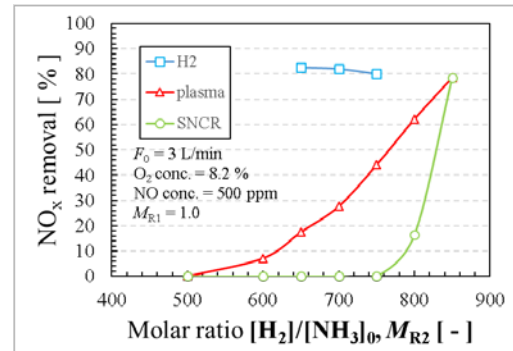


Fig. 4 Comparison of the biggest NO<sub>x</sub> removal efficiency in the optimum condition.

### IV. CONCLUSION

The experiment which finds the most suitable hydrogen addition amount in hydrogen addition de-NO<sub>x</sub> was made. We found the most suitable hydrogen addition amount at  $M_{R1} = 0.8, 0.9, 1.0$ ,  $T_R = 650 - 750$  °C. When the value of  $M_{R1}$  is fixed, the necessary hydrogen addition amount decreases with a rise of the reaction temperature. Since putting it in the same temperature range, when the value of  $M_{R1}$  becomes high, the most suitable hydrogen percentage decreases.

### REFERENCES

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